

Low Switching Frequency Pulse Width Modulation For Induction Motor Drives

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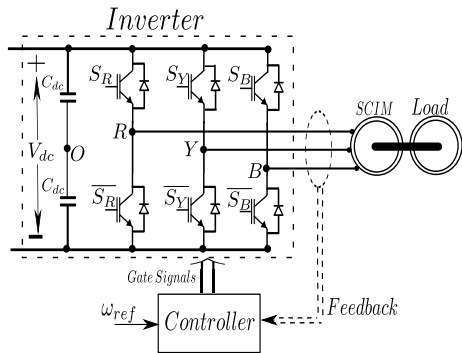
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Voltage Source Inverter Fed Induction Motor Drive

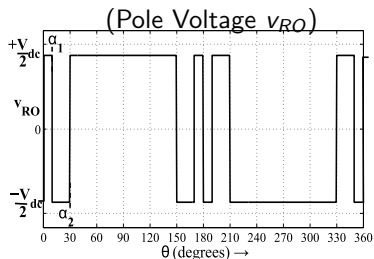


- Variable-amplitude variable-frequency voltage is generated to control the induction motor
- Switching frequency is generally much higher than maximum modulation frequency

- Switching frequency is low in high-power IM drives due to high switching energy losses
- In high-speed IM drives the maximum modulation frequency is quite high
- This work addresses the problems associated with such cases where the ratio of switching frequency to fundamental frequency (pulse number, P) is low

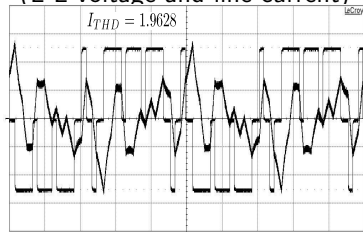


Problems with Low Pulse Number Applications

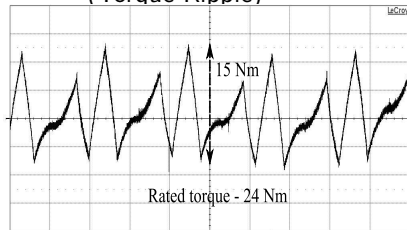


- Line-line voltage contains low-order voltage harmonics (i.e., 5th, 7th, 11th, 13th ...)
- These voltage harmonics produce current and fluxes of same order
- High harmonic distortion in line current
- Pulsating torque is very high

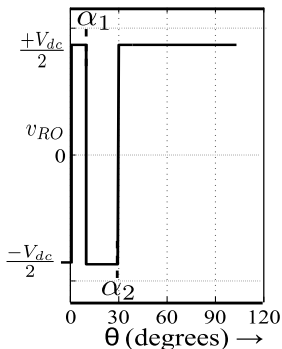
(L-L voltage and line current)



(Torque Ripple)



Minimization of Pulsating Torque



- Amplitude of n^{th} harmonic voltage component is given as:

$$V_n = \frac{2V_{dc}}{n\pi} (1 - 2 \cos(n\alpha_1) + 2 \cos(n\alpha_2))$$

- Selective harmonic elimination (SHE) PWM eliminates (N-1) voltage harmonics for N switching angles per quarter, e.g.

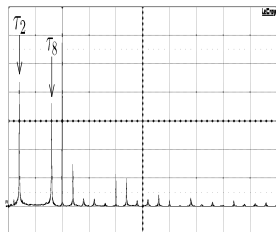
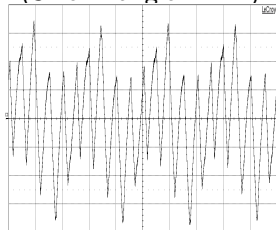
$$V_5 = (1 - 2 \cos(5\alpha_1) + 2 \cos(5\alpha_2)) = 0$$

- In optimal, α_1 and α_2 are selected such that $\| \frac{V_5}{5} + \frac{V_7}{7} \|$ is minimized subject to $(\frac{V_5}{5} = \frac{V_7}{7})$ for minimization of τ_6
- The fundamental voltage component is kept at desired level in both the cases
- The theory of torque harmonic minimization is extended to other pulse numbers also
- First (N-1) torque harmonics are minimized for N switching angles per quarter

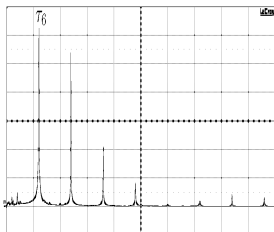
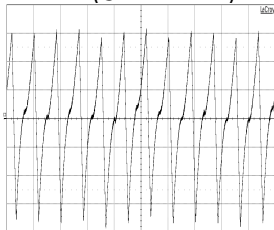


Experimental Comparison of Pulsating Torque for $P = 5$

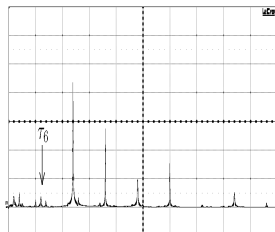
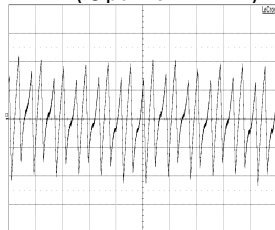
(Sine-Triangle PWM)



(SHE PWM)



(Optimal PWM)



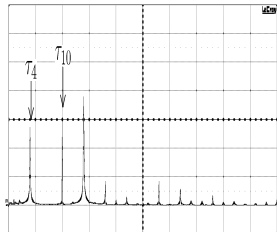
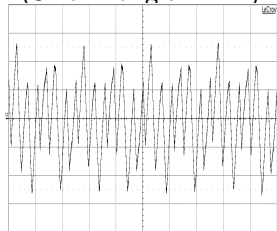
(scale: 5.0 Nm/div.; 5.0 ms/div. and 2.0 Nm/div.; 200 Hz/div.)($f_1 = 35$ Hz)

- Optimal PWM reduces the pk-pk torque ripple and sixth harmonic torque

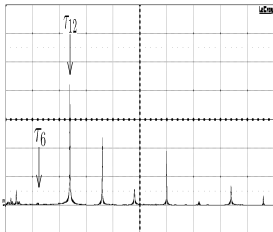
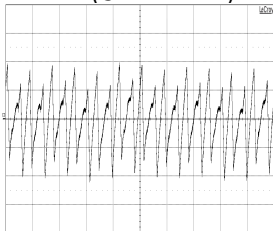


Experimental Comparison of Pulsating Torque for $P = 7$

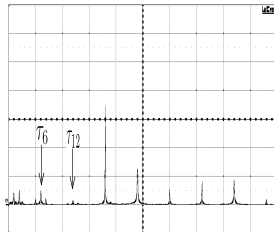
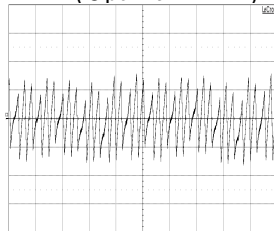
(Sine-Triangle PWM)



(SHE PWM)



(Optimal PWM)

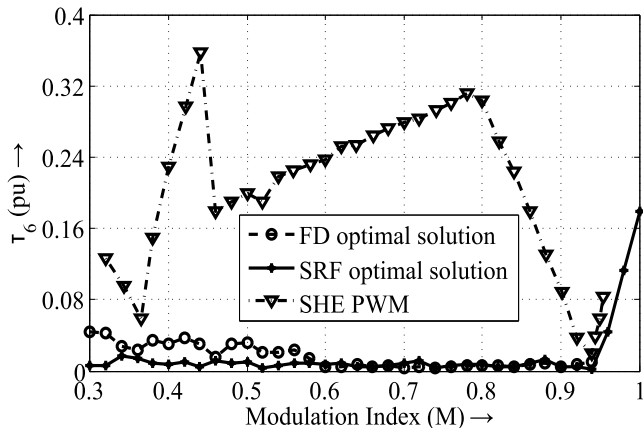


(scale: 5.0 Nm/div.; 5.0 ms/div. and 2.0 Nm/div.; 200 Hz/div.)($f_1 = 35$ Hz)

- Optimal PWM reduces the pk-pk torque ripple, sixth harmonic and twelfth harmonic torques



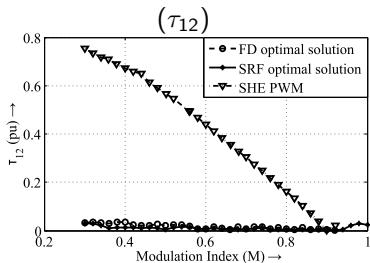
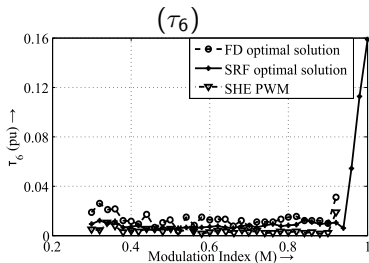
Experimental Comparison of Harmonic Torque for $P = 5$



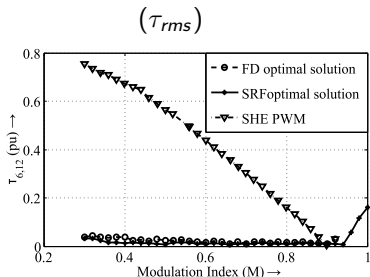
- Two optimal PWM methods are proposed - frequency domain and synchronous reference frame based
- Both are seen to reduce τ_6 as compared to SHE PWM, over wide range of speed



Experimental Comparison of Harmonic Torque for $P = 7$

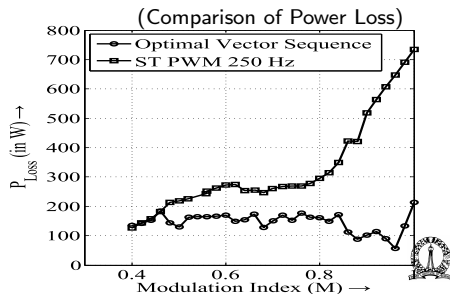
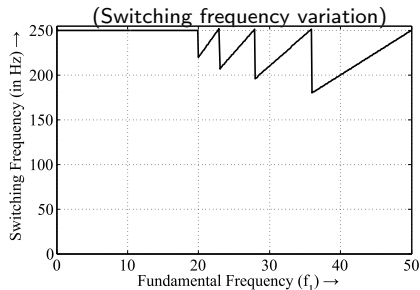
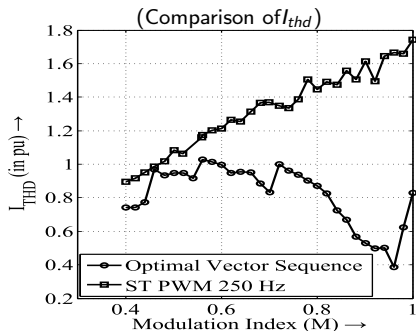


- SHE PWM eliminates τ_6 completely but τ_{12} is quite high
- Both optimal PWM reduce τ_{12} and combined RMS value of τ_6 and τ_{12} as compared to SHE PWM, over wide range of speed



Hybrid Optimal PWM For Induction Motor Drive

- Optimal switching sequence is obtained for various pulse numbers
- A hybrid optimal PWM with max switching freq (f_{sw}) of 250 Hz is proposed
- $f_1 < 20$ Hz - asyn ST PWM; $f_1 \geq 20$ Hz - optimal PWM



Contributions of The Thesis

- ⇒ Optimal PWM for minimization of line current THD is proposed
- ⇒ Optimal switching sequences in space vector are determined
- ⇒ Frequency domain and synchronous reference frame based methods are proposed to minimize a set of harmonic torques
- ⇒ The proposed scheme is extended to neutral point clamped three-level inverter
- ⇒ A method to predict the current and torque ripple based on PWM voltage is proposed
- ⇒ Closed-loop control of IM drive operated with asynchronous and synchronous ST PWM for switching frequency varying between 250Hz and 500Hz is achieved

...Thank you 